

# Non-reflecting boundary conditions and domain decomposition methods for industrial flow acoustics

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**Soutenance de thèse**  
**Nancy, June 16th, 2022**



X. Antoine



C. Geuzaine

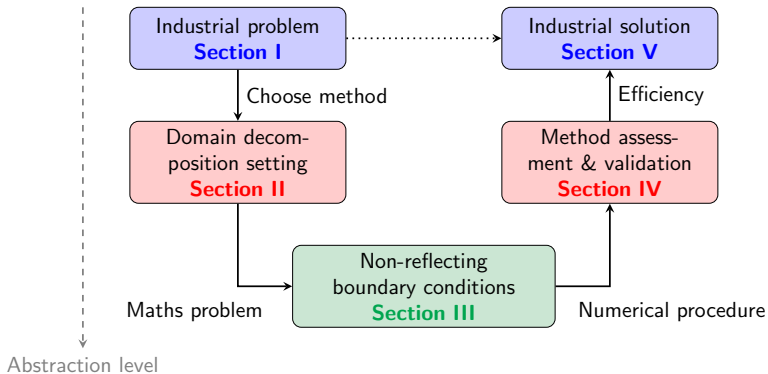


H. Bériot/P. Barabinot

# Outline

1. Industrial context
  - Physical models for sound propagation
  - Reaching the memory limit
  - Objective of the thesis
2. Domain decomposition framework
  - Method overview
  - Flow acoustics formulation
  - Updated objective
3. ABCs for heterogeneous and convected problems
  - Microlocal analysis
  - Application to the Linearized Potential Equation
  - Numerical examples
4. Application to non-overlapping domain decomposition
  - Heterogeneous waveguide problems
  - Convected problem in freefield
5. The 3D turbofan intake radiation problem
  - Numerical results for the turbofan problem
  - Solver weak scalability

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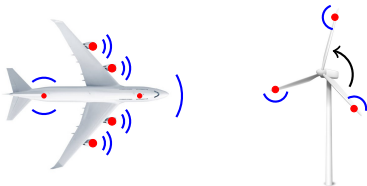
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# Industrial context

## Long term perspective

Predict noise from bodies in motion for the transport industry

## Computational (aero)acoustics



1. analyze & extract **sources**
2. understand **sound propagation**
3. find solutions (new material or design)

## Industrial objective

Provide a “*ready-to-use*” **sound propagation** simulation tool

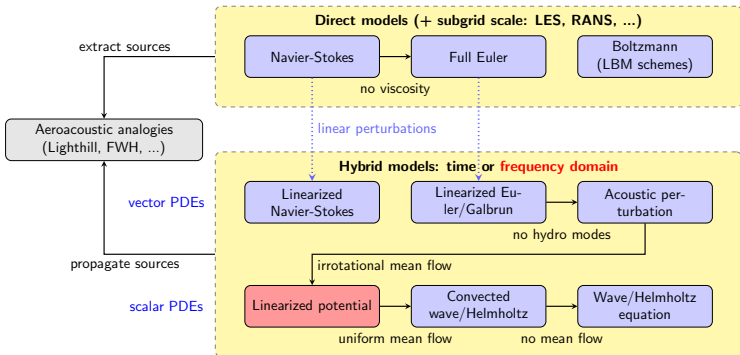
- suitable to modern computer architectures
- applicable to large, complex industrial problems

→ can serve as basis for optimization routines

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# Physical models for sound propagation



**Hybrid model** - solve mean flow and acoustic perturbations separately

- we choose the **time-harmonic Linearized Potential Equation**
- simple but accurate for single tones of turbofan engine intakes

# Physical model - Linearized Potential Equation

Scalar equation for the acoustic velocity potential  $\mathbf{v} = \nabla u$

## Linearized Potential Equation (LPE)

$$\rho_0(\mathbf{x}) \frac{D_0}{Dt} \left( \frac{1}{c_0(\mathbf{x})^2} \frac{D_0 u}{Dt} \right) - \nabla \cdot (\rho_0(\mathbf{x}) \nabla u) = f, \quad \frac{D_0}{Dt} = i\omega + \mathbf{v}_0(\mathbf{x}) \cdot \nabla$$

Helmholtz-type problem with **convection** and **heterogeneities**

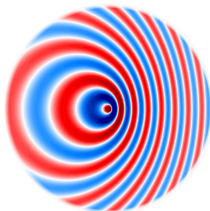
### Mathematical difficulties

- oscillatory, non-local solution
- complex valued, strongly indefinite with  $\omega$
- unbounded domain
- convection effects

does not converge with classical iterative methods [*Ernst, Gander 2012*]

→ use a **direct solver**

### Point source in a uniform flow



$$M = \|\mathbf{v}_0\| / c_0 = 0.6$$

$M < 1$  (Subsonic flow)



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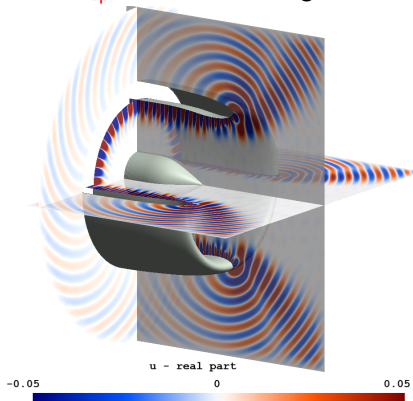
Solver weak scalability

# Reaching the high frequency limit

**Industrial example** : single tone turbofan intake radiation

**Current solver** : high-order  $p$ -FEM with direct solver (MUMPS)

$\omega_{\text{bpf}} \leftrightarrow \approx 25$  wavelengths



$\omega_{\text{bpf}}$ ,  $N_{\text{dofs}} = 10\text{M}$ ,  $\text{nnz} = 730\text{M}$   
Direct solver  $\rightarrow$  740 Gb of RAM

$\Downarrow$  increase  $\omega$  ?

$2 \times \omega_{\text{bpf}}$ ,  $N_{\text{dofs}} = 73\text{M}$ ,  $\text{nnz} = 5\text{B}$   
Direct solver  $\approx$  6 Tb of RAM ...

$\mathcal{O}(\omega^3)$  scaling in memory & time ...

can we distribute the memory cost ?  $\rightarrow$  domain decomposition

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# Objective of the thesis

## Industrial objective

Provide a (scalable) parallel solver to increase the upper frequency limit

## Starting point of the thesis

### Discretization

- high-order finite elements  
→ reduce discretization error (interpolation & dispersion)
- adaptive order based on *a-priori* error indicator [Bériot et al. 2016]  
→ less unknowns

### Parallelization

- algebraic parallelization is hard for Helmholtz problems
- instead, “divide and conquer” at the continuous (PDE) level  
→ domain decomposition
- lots of approaches, but common framework [Gander, Zhang 2019]

## Selected solution - 1st objective

Extend the non-overlapping optimal Schwarz domain decomposition framework [Boubendir et al. 2012] to the **Linearized Potential Equation**

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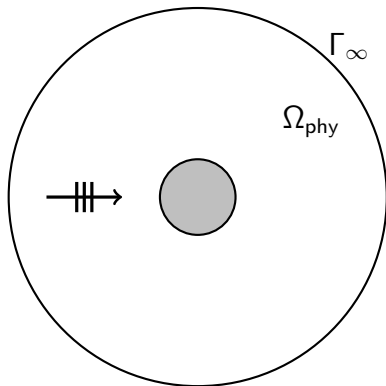
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# Overview - Non-overlapping optimal Schwarz

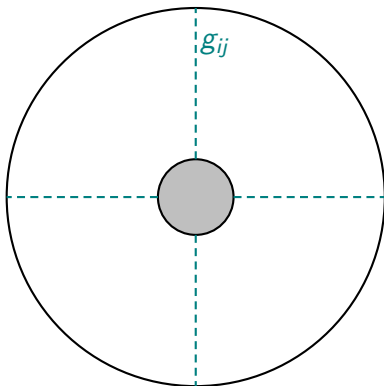
Toy example: disk scattering by a plane wave



# Overview - Non-overlapping optimal Schwarz

Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$   
into subdomains





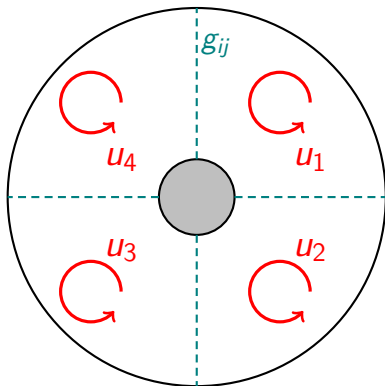
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## Toy example: disk scattering by a plane wave

- Partition  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$   
into **subdomains**

Iterate until convergence

1. Solve the **volume subproblems**  $u_i$  with boundary conditions



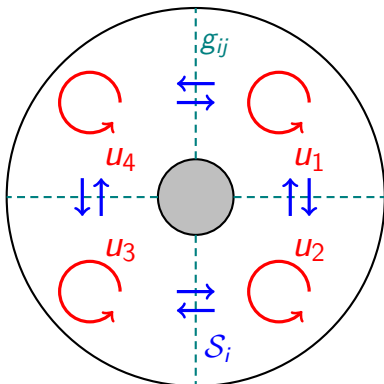
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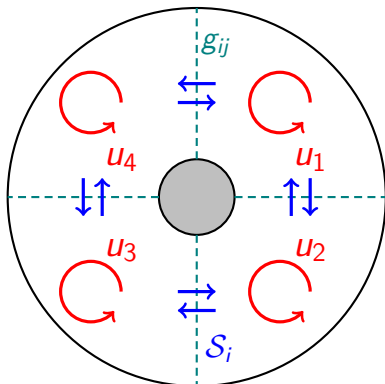
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- convergence ? [Després 1991]
- How to choose the operators  $(\mathcal{S}_i, \mathcal{S}_j)$  ?  $\rightarrow$  numerous works ...



Optimal convergence with the **Dirichlet-to-Neumann** operator

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# Flow acoustics formulation

In each subdomain  $\Omega_i$ , solve the boundary value problems

## Non-overlapping optimal Schwarz formulation

$$\begin{cases} \rho_0 \frac{D_0}{Dt} \left( \frac{1}{c_0^2} \frac{D_0 u_i}{Dt} \right) - \nabla \cdot (\rho_0 \nabla u_i) = 0 \text{ in } \Omega_i, \text{ (LPE)} \\ \rho_0 (1 - M_n^2) (\partial_{\mathbf{n}_i} u_i + \imath \tilde{\Lambda}^+ u_i) = 0, \text{ on } \Gamma_i^\infty \text{ (radiation condition)} \\ \rho_0 (1 - M_n^2) (\partial_{\mathbf{n}_i} u_i + \imath \mathcal{S}_i u_i) = g_{ij}, \text{ on } \Sigma_{ij}, \text{ (interface condition)} \end{cases}$$

Introduce the interface coupling on  $\Sigma_{ij}$

$$\begin{aligned} g_{ij} &= \rho_0 (1 - M_n^2) (-\partial_{\mathbf{n}_j} u_j + \imath \mathcal{S}_i u_j) \\ &= -g_{ji} + \imath \rho_0 (1 - M_n^2) (\mathcal{S}_i + \mathcal{S}_j) u_j := \mathcal{T}_{ji} g_{ji} + b_{ji} \end{aligned}$$

Rewrite the coupling as a linear system for  $\mathbf{g} = (g_{ij}, g_{ji})^T$

$$\underbrace{(\mathcal{I} - \mathcal{A})}_{\text{iteration matrix}} \underbrace{\mathbf{g}}_{\text{interface unknowns}} = \underbrace{\mathbf{b}}_{\text{physical sources}}, \quad \mathcal{A} = \begin{pmatrix} 0 & \mathcal{T}_{ji} \\ \mathcal{T}_{ij} & 0 \end{pmatrix}$$

$\mathcal{T}_{ij}$  and  $\mathcal{T}_{ji}$  are the **iteration operators**, and can be written in terms of  $\tilde{\Lambda}^+$

## Surface iteration operators

$$\mathcal{T}_{ji} = \frac{\mathcal{S}_i - \tilde{\Lambda}^+}{\mathcal{S}_j + \tilde{\Lambda}^+}, \quad \mathcal{T}_{ij} = \frac{\mathcal{S}_j + \tilde{\Lambda}^-}{\mathcal{S}_i - \tilde{\Lambda}^-}$$

Iteration matrix eigenvalues:  $\lambda_{(\mathcal{I}-\mathcal{A})} = 1 \pm \sqrt{\mathcal{T}_{ji}\mathcal{T}_{ij}}$

If we choose  $\mathcal{S}_i = \tilde{\Lambda}^+$  and  $\mathcal{S}_j = -\tilde{\Lambda}^-$ , we have optimal convergence

Parallel iterative algorithm for the process  $i$

Do in  $\Omega_i$  at iteration  $(n+1)$ ,  $\forall j \in D_i$

1. given  $g_{ij}^{(n)}$ , solve  $u_i^{(n+1)}$  in  $\Omega_i$ ,
2. update the  $(n+1)$  neighbourhood data through  $g_{ji}^{(n+1)} = -g_{ij}^{(n)} + \nu\rho_0 (1 - M_n^2) (\mathcal{S}_i + \mathcal{S}_j) u_i^{(n+1)}$  on  $\Sigma_{ij}$ ,

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$(\tilde{\Lambda}^+, -\tilde{\Lambda}^-)$  are **non-local DtN maps** for the LPE

→ design **sparse approximations**  $\mathcal{S}_i \approx \tilde{\Lambda}^+$  and  $\mathcal{S}_j \approx -\tilde{\Lambda}^-$

⇔ approximate **Schur complements** at the algebraic level

# Algebraic interpretation of domain decomposition

Global problem for two subdomains  $(i, j)$  with a common interface  $\Sigma$

$$\begin{pmatrix} \mathbb{K}_i^\Omega & 0 & \mathbb{K}_i^{\Omega, \Sigma} \\ 0 & \mathbb{K}_j^\Omega & \mathbb{K}_j^{\Omega, \Sigma} \\ \mathbb{K}_i^{\Sigma, \Omega} & \mathbb{K}_j^{\Sigma, \Omega} & \mathbb{K}_i^{\Sigma, \Sigma} + \mathbb{K}_j^{\Sigma, \Sigma} \end{pmatrix} \begin{pmatrix} u_i^\Omega \\ u_j^\Omega \\ u^\Sigma \end{pmatrix} = \begin{pmatrix} f_i^\Omega \\ f_j^\Omega \\ f_i^\Sigma + f_j^\Sigma \end{pmatrix}$$

Direct parallel solver  $\rightarrow$  block LU factorization per subdomain

$$\begin{pmatrix} \mathbb{I} & 0 & 0 \\ 0 & \mathbb{I} & 0 \\ \mathbb{K}_i^{\Sigma, \Omega} (\mathbb{K}_i^\Omega)^{-1} & \mathbb{K}_j^{\Sigma, \Omega} (\mathbb{K}_j^\Omega)^{-1} & \mathbb{I} \end{pmatrix} \begin{pmatrix} \mathbb{K}_i^\Omega & 0 & 0 \\ 0 & \mathbb{K}_j^\Omega & 0 \\ 0 & 0 & \mathbb{L} \end{pmatrix} \begin{pmatrix} \mathbb{I} & 0 & (\mathbb{K}_i^\Omega)^{-1} \mathbb{K}_i^{\Omega, \Sigma} \\ 0 & \mathbb{I} & (\mathbb{K}_j^\Omega)^{-1} \mathbb{K}_j^{\Omega, \Sigma} \\ 0 & 0 & \mathbb{I} \end{pmatrix},$$

The **Schur complement**  $\mathbb{L} = \mathbb{L}_i + \mathbb{L}_j$  is dense  $\Leftrightarrow$  **discrete DtN map**

$\rightarrow$  advances on dense Block Low-Rank factorization [*Amestoy et al. 2019*]

The non-overlapping Schwarz approach can be seen as an iterative solver for  $\mathbb{L}$  preconditioned by **interfaces conditions**

$\rightarrow$  **approximate block LU factorization** at the continuous level



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# Summary and updated objective

Non-overlapping domain decomposition for flow acoustics

- similar to the Helmholtz formulation, common framework
- quick convergence relies on sparse approximations of the DtN map  
⇔ Non-reflecting boundary conditions

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## Updated objective

Design non-reflecting boundary conditions for **heterogeneous** and **convected** time-harmonic problems

Two techniques were studied during the thesis

1. Absorbing Boundary Conditions (ABC) [*Marchner et al. SIAP 2022*],
2. Perfectly Matched Layers (PML) [*Marchner et al. JCP 2021*],

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## Next section

Focus on the construction of Absorbing Boundary Conditions

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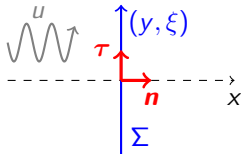
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# Microlocal analysis - DtN operator

Goal: find local approximations to the **Dirichlet-to-Neumann map**

## DtN operator on $\Sigma$

$$\widetilde{\Lambda}^+ : \begin{cases} H^{1/2}(\Sigma) \rightarrow H^{-1/2}(\Sigma) \\ u|_{\Sigma} \mapsto \partial_n u|_{\Sigma} = -i\widetilde{\Lambda}^+ u|_{\Sigma} \end{cases}$$



through pseudo-differential calculus

[Engquist and Majda 1977, 1979] [Antoine et al. 1999]

Example : 2D **heterogeneous** Helmholtz half-space problem

$$\begin{aligned} \mathcal{L} &= \rho_0^{-1} \partial_x (\rho_0 \partial_x) + \rho_0^{-1} \partial_y (\rho_0 \partial_y) + \omega^2 c_0^{-2} \\ &\underset{?}{\approx} \left( \partial_x + i \sqrt{\omega^2 c_0^{-2} + \rho_0^{-1} \partial_y (\rho_0 \partial_y)} \right) \left( \partial_x - i \sqrt{\omega^2 c_0^{-2} + \rho_0^{-1} \partial_y (\rho_0 \partial_y)} \right) \end{aligned}$$

We cannot formally factorize  $\mathcal{L}$  when  $\partial_x(\rho_0) \neq 0$  or  $\partial_x(c_0) \neq 0$

- Apply the principle to the **symbol**  $\lambda^+$  of  $\Lambda^+$
- work on polynomials in the co-tangent Fourier space  $\xi$

# Pseudo-differential operator

We define a differential operator of order  $m$ ,

$$\mathcal{P}(x, \partial_x) = \sum_{|\alpha| \leq m} (-i)^{|\alpha|} a_\alpha(x) \partial_x^\alpha, \quad x \in \mathbb{R}^d, \quad \alpha = (\alpha_1, \dots, \alpha_d) \in \mathbb{N}^d,$$

through its inverse Fourier representation  $\rightarrow$  more general framework

Pseudo-differential operator of order  $m$

$$\mathcal{P}(x, \partial_x)u(x) = \frac{1}{(2\pi)^d} \int_{\mathbb{R}^d} e^{ix \cdot \xi} p(x, \xi) \hat{u}(\xi) d\xi, \quad \xi \in \mathbb{R}^d$$

$p$  is the **symbol** of the operator  $\mathcal{P}$ , and is a smooth function of  $(x, \xi)$

Symbol of the operator  $\mathcal{P}$

$$p(x, \xi) = \sum_{|\alpha| \leq m} a_\alpha(x) \xi^\alpha, \quad \xi^\alpha = \xi_1^{\alpha_1} \dots \xi_d^{\alpha_d}$$

The highest order term is the **principal symbol**. We use **classical symbols**  $S_{cl}^m$

$$\left| \partial_x^\beta \partial_\xi^\alpha p(x, \xi) \right| \leq C(\alpha, \beta, K) (1 + |\xi|)^{m - |\alpha|}, \quad \forall (x, \xi) \in K \times \mathbb{R}^d,$$

Notations:

$$\mathcal{P} = \text{Op}(p) \in \text{OPS}^m, \quad p \in S_{cl}^m \Leftrightarrow \mathcal{P} \in \text{OPS}^m, \quad \text{OPS}^{-\infty} = \bigcap_{m \in \mathbb{R}} \text{OPS}^m$$



# Derivation of the DtN symbol - Helmholtz case

Nirenberg's factorization theorem: there exists  $(\Lambda^+, \Lambda^-) \in \text{OPS}^1$

$$\begin{aligned}\mathcal{L} &= (\partial_x + i\Lambda^-) (\partial_x + i\Lambda^+) \quad \text{mod OPS}^{-\infty} \\ &= \partial_x^2 + i(\Lambda^+ + \Lambda^-) \partial_x + i\text{Op}\{\partial_x \lambda^+\} - \Lambda^- \Lambda^+ \quad \text{mod OPS}^{-\infty}.\end{aligned}$$

Identify with the Helmholtz operator and get a system for  $(\Lambda^+, \Lambda^-)$

$$\begin{cases} \Lambda^+ + \Lambda^- = -i\rho_0^{-1} \partial_x(\rho_0) \\ (\Lambda^+)^2 + i\rho_0^{-1} \partial_x(\rho_0) \Lambda^+ + i\text{Op}\{\partial_x \lambda^+\} = \omega^2 c_0^{-2} + \rho_0^{-1} \partial_y(\rho_0 \partial_y) \end{cases}$$

→ "One-way" reformulation of the equation

"High frequency" asymptotic expansion for the total symbol  $\lambda^+$

$$\lambda^+ \sim \sum_{j=-1}^{\infty} \lambda_{-j}^+ = \lambda_1^+ + \lambda_0^+ + \lambda_{-1}^+ + \dots \quad (\text{classical symbol expansion})$$

Each symbol  $\lambda_{-j}^+$  is homogeneous in  $(\omega, \xi)^{-j}$ .

Once  $\lambda_1^+$  is fixed, the expansion is unique and can be computed formally

$$\lambda_1^+ = \sqrt{\omega^2 c_0^{-2} - \xi^2}, \quad \lambda_0^+ = -i \left( \frac{\partial_x(\rho_0)}{2\rho_0} + \frac{\xi \partial_y(\rho_0)}{2\rho_0 \lambda_1^+} + \frac{\omega^2 \partial_x(c_0^{-2})}{4(\lambda_1^+)^2} + \frac{\xi \omega^2 \partial_y(c_0^{-2})}{4(\lambda_1^+)^3} \right)$$

# Microlocal zones

Hyperbolic zone:  $\Re(\lambda_1^+) > 0 \rightarrow$  outgoing propagative waves

Elliptic zone:  $\Im(\lambda_1^+) < 0 \rightarrow$  outgoing evanescent waves

Rotation of the square-root branch-cut [Milinazzo et al. 1997]

$$\lambda_1^+ = e^{i\alpha/2} \sqrt{e^{-i\alpha}(\omega^2 c_0^{-2} - \xi^2)}, \quad \alpha \in [0, -\pi], \quad (+i\omega t \text{ convention})$$

The branch-cut is rotated by an angle  $\alpha$  in the complex plane

- Hyperbolic zone:  $\omega c_0^{-1} > |\xi| \rightarrow \alpha = 0$ ,
- Elliptic zone:  $\omega c_0^{-1} < |\xi| \rightarrow \alpha = -\pi$ ,
- Grazing zone:  $\omega c_0^{-1} = |\xi|$ , ill-posed problem

In practice we choose  $\alpha \in (0, -\pi/2]$

$\rightarrow$  trade-off to capture both propagative and evanescent waves

# Summary - building the DtN approximation

Approximate DtN operator with the  $M$  first symbols

$$\partial_{\mathbf{n}} u = -i\Lambda_M^+ u, \quad \Lambda_M^+ = \sum_{j=-1}^{M-2} \text{Op}(\lambda_{-j}^+)$$

Take the trace on the boundary  $\Sigma$  to get  $\tilde{\Lambda}_M^+$ , such that

$$\left(\tilde{\Lambda}^+ - \tilde{\Lambda}_M^+\right) \in \text{OPS}^{1-M}$$

## Technical difficulties

- the formal computation of  $\lambda_{-j}^+$  can be involved (PDE dependent)
- the operator  $\text{Op}(\lambda_{-j}^+)$  is in general not unique and still non-local
- limited *a priori* to smooth variations of  $\rho_0$  and  $c_0$

## Next step - original contribution

- Apply the theory to flow acoustics

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# DtN symbol computation

**Step 1** Nirenberg's factorization theorem for the flow acoustics operator

$$\mathcal{L} = \frac{D_0}{Dt} \left( \frac{1}{c_0^2} \frac{D_0}{Dt} \right) - \rho_0^{-1} \nabla \cdot (\rho_0 \nabla), \quad \frac{D_0}{Dt} = i\omega + \mathbf{v}_0 \cdot \nabla$$

We note  $M_x = v_{0,x}/c_0$ ,  $M_y = v_{0,y}/c_0$ ,  $M = \|\mathbf{v}_0\|/c_0$ ,  $k_0 = \omega/c_0$

**Step 2** Derive an operator equation for the outgoing characteristic  $\Lambda^+$

$$(1 - M_x^2) (\Lambda^+)^2 - i(\mathcal{A}_1 + \mathcal{A}_0) \Lambda^+ + i(1 - M_x^2) \text{Op} \{ \partial_x \lambda^+ \} = \mathcal{B}_2 + \mathcal{B}_1 \text{ mod OPS}^{-\infty}$$

with  $i(\Lambda^+ + \Lambda^-) = (\mathcal{A}_1 + \mathcal{A}_0) / (M_x^2 - 1)$ ,  $\sigma(\mathcal{A}_j), \sigma(\mathcal{B}_j) \in \mathcal{S}_{cl}^j$ ,  $j = \{0, 1, 2\}$

**Step 3** Classical symbol expansion, identify 2nd order terms in  $(\omega, \xi)$

DtN principal symbol for flow acoustics

$$\lambda_1^\pm = \frac{1}{1 - M_x^2} \left[ -M_x (k_0 - \xi M_y) \pm \sqrt{k_0^2 - 2k_0 M_y \xi - (1 - M^2) \xi^2} \right]$$

Microlocal zones delimited by  $\omega c_0^{-1} = (M_y \pm \sqrt{1 - M_x^2}) \xi$

Subsonic flow  $M < 1 \Rightarrow$  two characteristic lines of opposite sign

# DtN symbol computation

## Step 3 - bis

Compute the next symbols of the expansion ...

$$\lambda_0^+ = \frac{\sigma(\mathcal{B}_1) + i\sigma(\mathcal{A}_0)\lambda_1^+ + i(1 - M_x^2) (\partial_\xi \lambda_1^+ \partial_y \lambda_1^+ - \partial_x \lambda_1^+)}{2\sqrt{k_0^2 - 2k_0 M_y \xi - (1 - M^2)\xi^2}}.$$

If  $M_y = 0$  we have the simplification

Zereth order symbol for an  $x$ -oriented flow

$$\lambda_0^+ = -i \frac{\partial_x(\rho_0)}{2\rho_0} \frac{k_0^2 - \xi^2}{k_0^2 - (1 - M_x^2)\xi^2} + i \frac{\partial_x(c_0)}{2c_0} \frac{k_0^2 + M_x^2 \xi^2}{k_0^2 - (1 - M_x^2)\xi^2}$$

$$\lambda_{-1}^+ = \dots, \quad \lambda_{-2}^+ = \dots$$

# Going back to the operator level

**Final step** go back to the operator level

Approximate DtN operator

$$\begin{aligned}\tilde{\Lambda}_1^+ &= \text{Op}(\lambda_1^+) = \frac{k_0}{1-M_n^2} \left( -M_n + iM_n M_\tau \frac{\nabla_\Sigma}{k_0} + \sqrt{1+X} \right) \\ X &= -2iM_\tau \frac{\nabla_\Sigma}{k_0} + (1-M^2) \frac{\Delta_\Sigma}{k_0^2}, \quad M = \|\mathbf{v}_0\| / c_0\end{aligned}$$

For the half-space problem with constant coefficients

$$\tilde{\Lambda}^+ = \tilde{\Lambda}_1^+ \quad \text{mod } \text{OPS}^{-\infty}$$

For variable coefficients and/or in the tangent plane approximation  $(\mathbf{n}, \tau)$

$$\tilde{\Lambda}^+ = \tilde{\Lambda}_1^+ \quad \text{mod } \text{OPS}^0$$

The choice for  $\text{Op}(\lambda_1^+)$  is not unique, but has  $\lambda_1^+$  as principal symbol

**Issue:** the approximate DtN map  $\tilde{\Lambda}_1^+$  is still non-local  
→ we need a local representation for  $\sqrt{1+X}$

# Localization procedure

High-frequency approximation for  $\sqrt{1+X}$ ,  $X \rightarrow 0$  ( $\omega \rightarrow +\infty$ )  
Use complexified Padé or Taylor approximations ( $N, \alpha$ ) for

$$\Lambda(Z) = e^{i\alpha/2} \sqrt{1+Z}, \quad Z = [e^{-i\alpha}(1+X) - 1],$$

with  $Z$  a surfacic second order differential operator on the boundary  $\Sigma$

## Taylor approximation

$$\Lambda(Z) \approx e^{i\alpha/2} \sum_{\ell=0}^N \binom{1/2}{\ell} (e^{-i\alpha}(1+X) - 1)^\ell$$

## Padé approximation

$$\Lambda(Z) \approx K_0(\alpha) + \sum_{\ell=1}^N A_\ell(\alpha) X (1 + B_\ell(\alpha) X)^{-1}$$

## Resulting local Absorbing Boundary Conditions

Complex Padé approximants:  $\tilde{\Lambda}_1^+ \rightarrow ABC_1^{N,\alpha}$

Complex Taylor approximants:  $\tilde{\Lambda}_1^+ \rightarrow ABC_1^{T0,\alpha}$  and  $ABC_1^{T2,\alpha}$



# High-order FEM implementation

Discretization on a conformal, high-order  $H^1$ -basis

Weak formulation for the linearized potential equation

$$\forall v \in V \subseteq H^1(\Omega),$$
$$\int_{\Omega} \left[ \rho_0 \nabla u \cdot \overline{\nabla v} - \frac{\rho_0}{c_0^2} \frac{D_0 u}{Dt} \overline{\frac{D_0 v}{Dt}} \right] d\Omega + i \int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Omega} f \bar{v} d\Omega$$

The boundary operator  $\mathcal{G}$  takes the same form as in the Helmholtz case

$$\int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Sigma} e^{i\alpha/2} \rho_0 k_0 \sqrt{1 + Z} u \bar{v} d\Sigma$$

$$\text{with } Z = e^{-i\alpha} \left( 1 - 2iM_{\tau} \frac{\nabla_{\Sigma}}{k_0} + (1 - M^2) \frac{\Delta_{\Sigma}}{k_0^2} \right) - 1$$

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**Taylor approximants:**  $ABC_1^{T2, \alpha}$

$$\begin{aligned} \int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma &= \cos(\alpha/2) \int_{\Sigma} \rho_0 k_0 u \bar{v} d\Sigma \\ &+ e^{-i\alpha/2} \left( \int_{\Sigma} \rho_0 M_{\tau} \nabla_{\Sigma} u \bar{v} d\Sigma - \int_{\Sigma} \rho_0 \frac{(1 - M^2)}{2k_0} \nabla_{\Sigma} u \nabla_{\Sigma} \bar{v} d\Sigma \right) \end{aligned}$$

# High-order FEM implementation - Padé case

**Padé approximants:**  $ABC_1^{N,\alpha}$

$$\int_{\Sigma} \mathcal{G} u \bar{v} d\Sigma = \int_{\Sigma} \rho_0 k_0 K_0(\alpha) u \bar{v} d\Sigma + \sum_{\ell=1}^N \int_{\Sigma} \rho_0 k_0 A_{\ell}(\alpha) X \varphi_{\ell} \bar{v} d\Sigma$$

with  $X = -2iM_{\tau} \frac{\nabla_{\Sigma}}{k_0} + (1 - M^2) \frac{\Delta_{\Sigma}}{k_0^2}$

Introduce **auxiliary fields**  $\varphi_{\ell} = (1 + B_{\ell}X)^{-1}u$  to obtain a **sparse** discretization of inverse operators

→ augmented system of  $N$  surfacic equations

$$\forall \ell \in [1, N], \forall v_{\ell} \in H^1(\Sigma)^N, \quad \int_{\Sigma} (1 + B_{\ell}(\alpha)X) \varphi_{\ell} \bar{v}_{\ell} d\Sigma = \int_{\Sigma} u \bar{v}_{\ell} d\Sigma$$

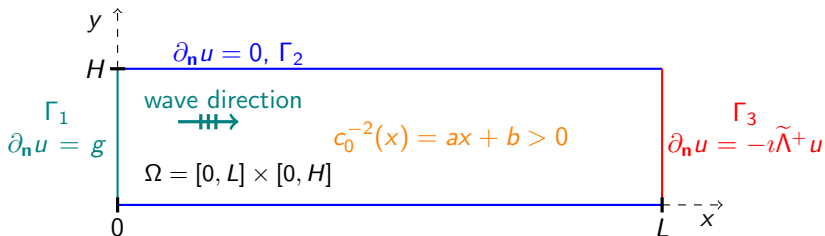
Global linear system of size  $[N_{\text{dof},\Omega} + (N \times N_{\text{dof},\Sigma})]$

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# Longitudinal heterogeneous waveguide

Example 1: No mean flow, single mode propagation in a heterogeneous waveguide:  $\rho_0 = 1$ ,  $c_0(x, y) = c_0(x)$



Single mode analytic solution for a linear profile

$$u_{\text{ex}}^n(x, y) = \cos(k_y y) \text{Ai} \left( e^{-\frac{2+\pi}{3}} \frac{k_y^2 - \omega^2(ax+b)}{(a\omega^2)^{2/3}} \right), \quad k_y = \frac{n\pi}{H}, \quad n \in \mathbb{N}$$

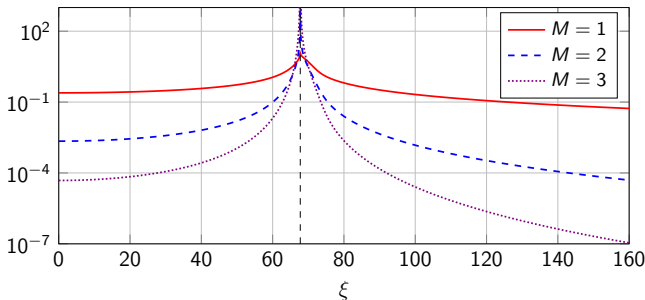
# Approximation at the symbol level

$c_0^{-2}(x) = 5x + 0.1$ ,  $L = 1$  at fixed frequency  $\omega = 30$

## Analytic total symbol

$$\lambda^+ = -i e^{-\frac{2i\pi}{3}} (a\omega^2)^{1/3} \frac{\text{Ai}'(\zeta)}{\text{Ai}(\zeta)}, \quad \zeta = e^{-\frac{2i\pi}{3}} \frac{\xi^2 - \omega^2(aL+b)}{(a\omega^2)^{2/3}}$$

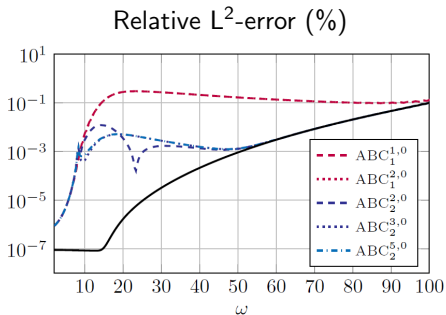
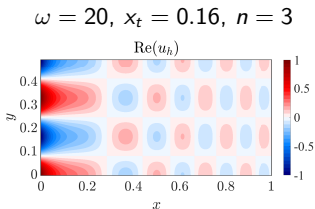
$$\left| \lambda^+ - \sum_{j=-1}^{M-2} \lambda_{-j}^+ \right|$$



- singularity in the grazing regime  $\xi \approx \omega c_0^{-1}$

# Numerical results

$ABC_M^{N,\alpha}$ : Local Padé approximation of  $\tilde{\Lambda}_M^+$  with rotation branch-cut  $\alpha$



Use the derivative of  $c_0 \Rightarrow$  more accurate ABC:  $ABC_2^{N+1,\alpha} > ABC_1^{N,\alpha}$

Gain of  $\approx$  two order of magnitude

Precision limited by the DtN symbol truncation

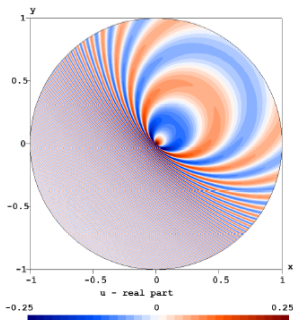
Similar conclusion with Taylor approximations of order 0 and 2

# Point source convection in free field

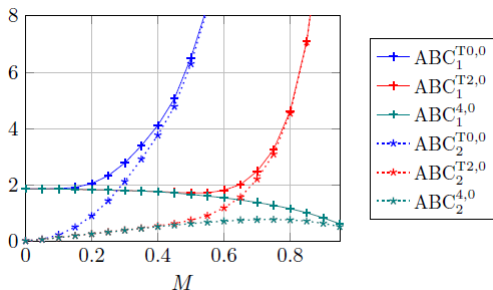
Example 2:  $\rho_0 = c_0 = 1$ , point source in uniform mean flow of angle  $\theta$   
Padé approximants  $\rightarrow ABC_1^{N,\alpha}$ , Taylor approximants  $\rightarrow ABC_1^{T0,\alpha}$ ,  $ABC_1^{T2,\alpha}$   
Attempt to incorporate curvature effects from  $\lambda_0^+$  (circle of radius  $R$ )

$$ABC_2 = ABC_1 + (1 - M^2)/(2R)$$

$k_0 = 6\pi, M = 0.95, R = 1, \theta = \pi/4$



Relative  $L^2$ -error (%)



$ABC_1^{N,\alpha}$  is robust for high Mach numbers - wavelength ratio  $(1 + M)/(1 - M)$



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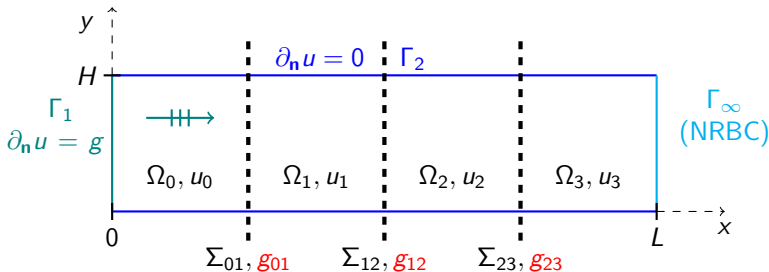
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# Waveguide problem with straight partitions

Domain partition:  $\Omega = \bigcup_{i=0}^{N_{\text{dom}}-1} \Omega_i$ ,  $\Sigma_{ij} = \overline{\partial\Omega_i} \cap \partial\Omega_j$ ,  $j \neq i$



Two test cases

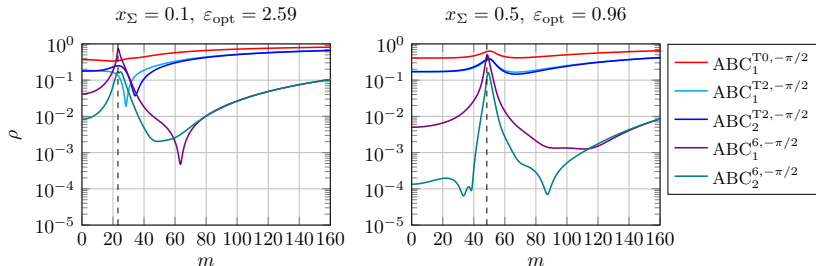
1. Linear speed of sound profile :  $c_0^{-2}(x) = ax + b$
2. Transverse density and/or speed of sound :  $c_0(y), \rho_0(y)$

# Longitudinal heterogeneous waveguide

Reminder - ABC study

- $ABC_2^{N+1,\alpha} > ABC_1^{N,\alpha}$
- Precision limited by the truncation of the total DtN symbol  $\lambda^+$

Plot theoretical convergence radius  $\rho(m, x) = \sqrt{|\mathcal{T}_{ij}^m \mathcal{T}_{ji}^m|}$  at  $\omega = 30$



DDM waveguide study - input boundary condition with the 21 first modes

$N_{\text{dom}}$	$ABC_1^{T0,\alpha}$	$ABC_1^{T2,\alpha}$	$ABC_1^{6,\alpha}$	$ABC_2^{6,\alpha}$
8	76 (dnc)	51 (87)	34 (37)	24 (27)

Table: GMRES(Jacobi) iterations to  $10^{-6}$  at  $\omega = 40, \alpha = -\pi/4, d_\lambda = 12$

# Transverse heterogeneous waveguide

Gaussian waveguide:  $c_0(y) = 1.25 \left(1 - 0.4e^{-32(y-H/2)^2}\right)$ ,  $\rho_0(y) = c_0^2(y)$

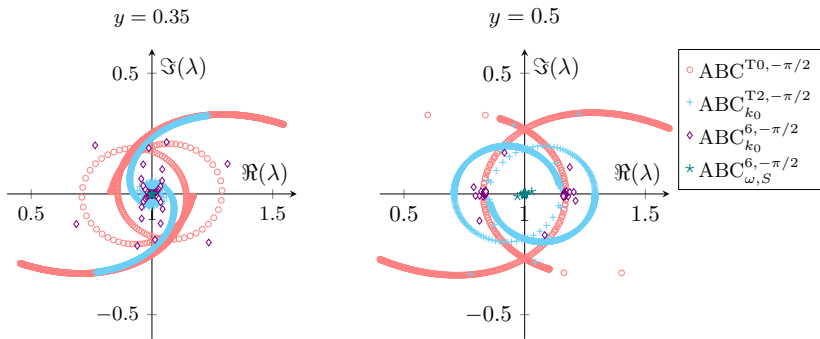


Figure: Theoretical eigenvalues of the DDM iteration matrix,  $\omega = 50$

- Usual Padé approximation (classical principal symbol) -  $\mathcal{S}_i = ABC_{k_0}^{N, \alpha}$
- New approximation (semi-classical principal symbol) -  $\mathcal{S}_i = ABC_{\omega, S}^{N, \alpha}$   
→ almost perfect clustering

# Illustration for a Gaussian waveguide

DDM - large PML on  $\Gamma_\infty$  - input mode  $n = 4$  -  $N_{\text{dom}} = 8$

$N_{\text{dom}}$	$\text{ABC}_{k_0}^{\text{T}0, -\pi/4}$	$\text{ABC}_{k_0}^{\text{T}2, -\pi/4}$	$\text{ABC}_{k_0}^{4(8), -\pi/4}$	$\text{ABC}_\omega^{4(8), -\pi/4}$
8	111	74	42 (42)	20 (8)

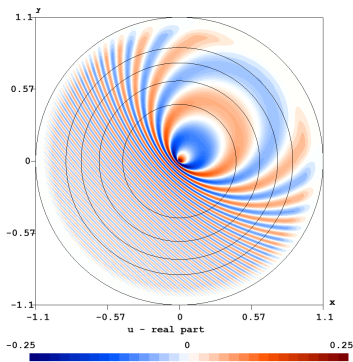
Table: GMRES iterations to  $10^{-6}$  at  $\omega = 160, d_\lambda = 24$

Convergence in  $N_{\text{dom}}$  iterations  $\rightarrow$  continuous block LU factorization

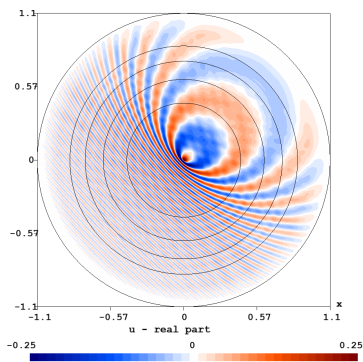
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# Convected problem in freefield - circular interfaces



(a)  $ABC_1^{4, -\pi/4}$ ,  $\mathcal{E}_{L^2} = 1.7\%$



(b)  $ABC_1^{T2, -\pi/4}$ ,  $\mathcal{E}_{L^2} = 24\%$

Numerical solution after 4 GMRES iterations.

Parameters:  $M = 0.9$ ,  $\theta = \pi/4$ ,  $p = 9$ ,  $d_\lambda = 8$ ,  $N_{\text{dom}} = 5$ ,  $\omega = 6\pi$ .

$L^2$ -error "PML-analytical solution" : 0.8%.

Padé conditions are robust for **high Mach numbers**



# Mach number variation - circular interfaces

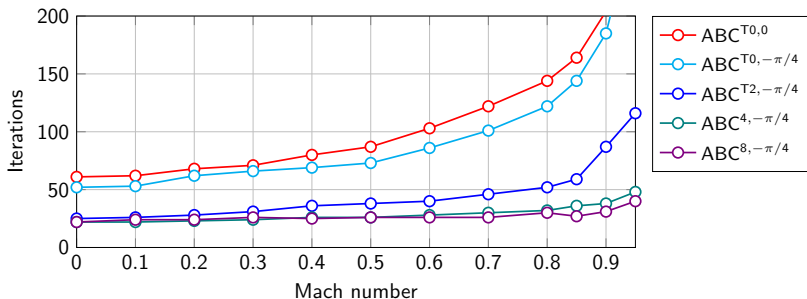
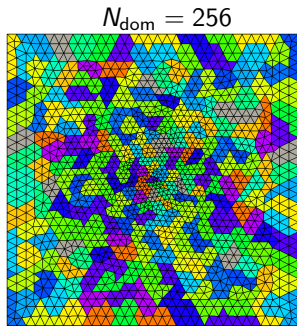


Figure: GMRES iterations to reach  $10^{-6}$  for  $N_{\text{dom}} = 5$ ,  $\omega = 6\pi$

- Only Padé conditions are robust for high Mach numbers
- Layered partition: iteration number increases as  $\mathcal{O}(N_{\text{dom}})$

## Automatic partitioning

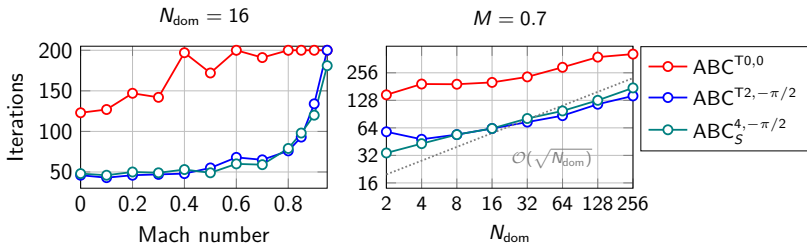
- Cross-points  
→ harder to design ABCs
- Industrial need - good load balancing between subproblems
- Shorter connectivity graph -  $\mathcal{O}(\sqrt{N_{\text{dom}}})$



**Corner problem** : use Padé approximants on edges with Sommerfeld-type condition on corners → approximate corner treatment  
Resulting condition  $ABC_S^{N,\alpha}$

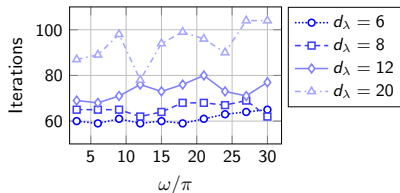
Are such Padé conditions still effective for domain decomposition ?

# Numerical study - arbitrary decomposition



GMRES iterations to reach  $10^{-6}$  for  $\omega = 6\pi$ ,  $d_\lambda = 8$

- lost of robustness for high Mach numbers
- $ABC^{T2,-\pi/2}$ ,  $ABC_S^{4,-\pi/2}$   
→ similar performance
- $ABC^{T2,-\pi/2}$  is cheaper (and easier) to implement



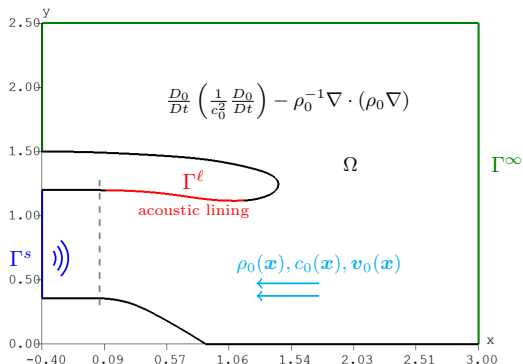
$M = 0.7$ ,  $N_{\text{dom}} = 16$ ,  $ABC^{T2,-\pi/2}$

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# The boundary value problem

Given a **flight configuration (mean flow)**, predict the radiated noise from the fan, at multiples of the blade passing frequency  $\omega_{\text{bpf}}/(2\pi) = 1300$  Hz



## Boundary conditions

- Ingard-Myers on  $\Gamma^\ell$
- PML (active) on  $\Gamma^s$
- Fixed annular Bessel mode on  $\Gamma^s$
- PML (passive) on  $\Gamma^\infty$

The mean flow is pre-computed and **interpolated** on the acoustic mesh

# Outline

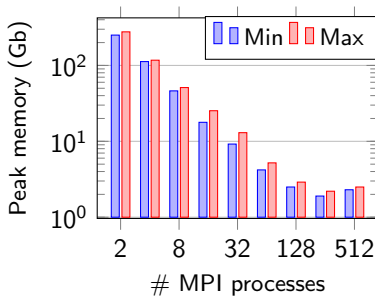
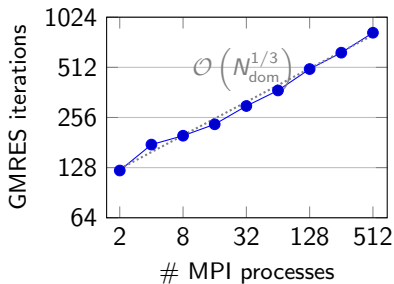
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# DDM for the 3D turbofan problem

$\omega_{\text{bpf}} - N_{\text{dofs}} = 10\text{M} - \text{nnz} = 730\text{M}$

$\approx 25$  wavelengths in  $\Omega$

Direct solver  $\rightarrow$  740 Gb RAM for factorization



Parallel GmshDDM solver (mono-thread)

From  $N_{\text{dom}} > 128$ , under 10 minutes and less than 3Gb per process

Iterations for  $N_{\text{dom}} = 64$

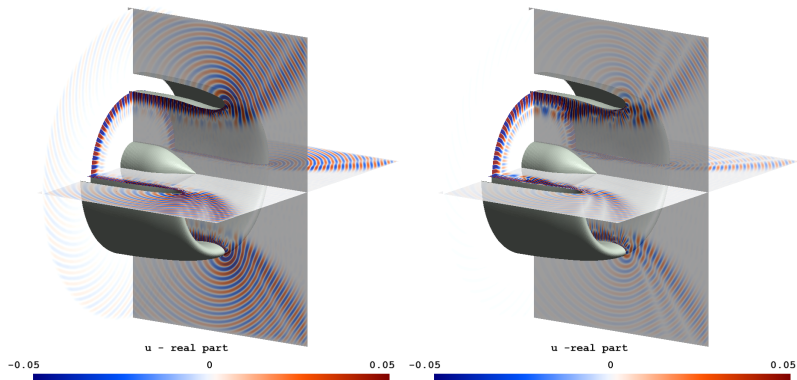
- $\text{ABC}^{\text{T}2, -\pi/2}$ : 372 GMRES iterations to  $10^{-6}$
- $\text{ABC}^{\text{T}0, 0}$ :  $> 2000$  GMRES iterations to reach  $10^{-3}$

# DDM for the 3D turbofan problem

$2 \times \omega_{\text{bpf}} - N_{\text{dofs}} = 73\text{M} - \text{nnz} = 5\text{B} \quad \approx 50 \text{ wavelengths in } \Omega$

Parallel GmshDDM solver (mono-thread),  $N_{\text{dom}} = \# \text{ MPI} = 128$

→ 2hours 3min, 26 Gb peak memory, 712 GMRES iterations (with lining)



**Figure:** Real part of the acoustic velocity potential for the mode (48, 1) at  $2 \times \omega_{\text{bpf}}$  (2600 Hz) without (left) and with (right) acoustic lining treatment.



# Outline

1. Industrial context
  - Physical models for sound propagation
  - Reaching the memory limit
  - Objective of the thesis
2. Domain decomposition framework
  - Method overview
  - Flow acoustics formulation
  - Updated objective
3. ABCs for heterogeneous and convected problems
  - Microlocal analysis
  - Application to the Linearized Potential Equation
  - Numerical examples
4. Application to non-overlapping domain decomposition
  - Heterogeneous waveguide problems
  - Convected problem in freefield
5. The 3D turbofan intake radiation problem
  - Numerical results for the turbofan problem
  - Solver weak scalability

# Weak scalability assessment

3D Helmholtz problem with  $d_\lambda = 7.5$  points per wavelength

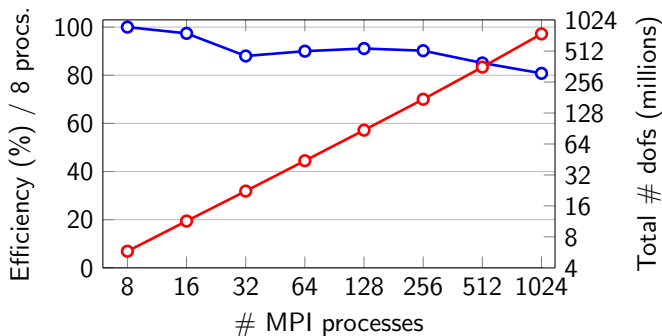


Figure: Weak scaling timing for 1 iteration

## Limitations

- memory load balancing: [20-34] Gb for 1024 processes
- number of iterations scales as  $\mathcal{O}(N_{\text{dom}}^{1/3})$  in 3D

## Distributed memory solver for high frequency flow acoustics

1. Extension of a generic domain decomposition method to flow acoustics
2. Development of non-reflecting boundary conditions: ABCs and PMLs
  - ▶ extension to media with heterogeneities and convection
  - ▶ general PML procedure for flow acoustics
3. Code development (*GmshDDM*), validation and assessment of ABCs in a domain decomposition context
4. Proof of concept - turbofan intake
5. 80% scalability up to 700M high-order unknowns and 1024 MPI processes

## Limitations

- The iterative solver does not scale with  $N_{\text{dom}}$  → requires coarse space
- Theoretical limitations - corners, curved boundaries, PML-DDM, etc.

## Future developments

- Extension to Pierce equation → turbofan exhaust [*Spieser, Bailly 2020*]
- Modern discretization techniques such as HDG or HHO [*Li et al. 2013*]
- Interfaces through the mesh → immersed transmission conditions

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Thank you !